

Optimization of the Emitting Coil of a Hardware-Software Complex for Study of Low-Frequency Electromagnetic Radiation's Shielding Effectiveness

O.D. Kanafyev¹, A.V. Trukhanov¹, T.I. Zubar¹, S.A. Chizhik², S.S. Grabchikov¹

¹Scientific and Practical Materials Research Center of the National Academy of Sciences of Belarus,
P. Brovki str., 19, Minsk 220072, Belarus

²National Academy of Sciences of Belarus,
Nezavisimosty Ave., 66, Minsk 220072, Belarus

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Abstract

Optimization of the radiation coil of the hardware-software complex for studying the effectiveness of shielding of low-frequency electromagnetic radiation will make it possible to assess the effectiveness of shielding coatings at a higher level. This fact will make it possible to develop coatings with improved characteristics. The purpose of this work was to determine the optimal characteristics of the emitting coil which will ensure its stable operation and magnetic field strength in the frequency range up to 100 kHz.

The parameters of the manufactured samples, such as inductance (L), active (R) and total resistance (Z), were obtained using an *MNIP I E7-20* emittance meter. In practice, the coils with the optimal parameters calculated theoretically were connected to a current source and amplifier. To detect electromagnetic radiation, a multilayer inductor connected to a *UTB-TREND 722-050-5* oscilloscope was used as a signal receiver.

The results of measurements showed that the resistance of multilayer coils is approximately 1000 times higher than that of single-layer coils. Also, for multilayer coils, an avalanche-like increase in total resistance is observed starting from a frequency of 10 kHz, while for single-layer coils there is a uniform increase in total resistance over the entire frequency range up to 100 kHz.

The paper presents results of research on the correlation of the performance of single-layer and multilayer inductors depending on their parameters in the frequency range from 20 Hz to 100 kHz. Values of the voltage required to provide the magnetic field strength of 1, 5, 20 Oe at 25 Hz and 100 kHz have been calculated. After analyzing the data obtained, the optimal parameters of the inductor were found which ensure stable performance in the frequency range up to 100 kHz.

Keywords: inductor coil, shielding, electromagnetic emitting.

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Адрес для переписки:

Канафьев О.Д.
НППЦ НАН Беларуси по материаловедению,
ул. П. Бровки, 19, г. Минск 220072, Беларусь
e-mail: olegkan96@mail.ru

Address for correspondence:

Kanafyev O.D.
Scientific and Practical Materials Research Center of the National
Academy of Sciences of Belarus,
P. Brovki str., 19, Minsk 220072, Belarus
e-mail: olegkan96@mail.ru

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Оптимизация излучающей катушки программно-аппаратного комплекса для исследования эффективности экранирования низкочастотного электромагнитного излучения

О.Д. Канафьев¹, А.В. Труханов¹, Т.И. Зубарь¹, С.А. Чижик², С.С. Грабчиков¹

¹Научно-практический центр Национальной академии наук Беларуси по материаловедению,
ул. П. Бровки, 19, г. Минск 220072, Беларусь

²Национальная Академия наук Беларуси,
пр-т Независимости, 66, г. Минск 220072, Беларусь

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Оптимизация излучающей катушки программно-аппаратного комплекса для исследования эффективности экранирования низкочастотного электромагнитного излучения позволит на более качественном уровне оценивать эффективность экранирующих покрытий. Данный факт даст возможность разрабатывать покрытия с улучшенными характеристиками. Целью данной работы являлось определение оптимальных характеристик излучающей катушки, которые обеспечат её стабильную работу и напряжённость магнитного поля в частотном диапазоне до 100 кГц.

Параметры изготовленных образцов, такие как индуктивность, активное и общее сопротивление, были получены, используя измеритель иммитанса МНИПИ Е7-20. На практике катушки с оптимальными параметрами, вычисленными теоретически, были подключены к источнику и усилителю тока. Для детектирования электромагнитного излучения в качестве приёмника сигнала использовалась многослойная катушка индуктивности, подключённая к осциллографу *UTB-TREND 722-050-5*.

Результаты измерений показали, что сопротивление многослойных катушек приблизительно в 1000 раз больше сопротивления однослойных. Также у многослойных катушек наблюдается лавинообразный рост общего сопротивления, начиная с частоты 10 кГц, в то время как у однослойных катушек происходит равномерный рост общего сопротивления на всём диапазоне частот до 100 кГц.

Представлены результаты исследований корреляции рабочих характеристик однослойных и многослойных катушек индуктивности в зависимости от их параметров в частотном диапазоне от 20 Гц до 100 кГц. Рассчитаны значения напряжения, необходимого для обеспечения напряжённости магнитного поля 1, 5, 20 Э при 25 Гц и 100 кГц. Проанализировав полученные данные, найдены оптимальные параметры катушки индуктивности, обеспечивающие стабильные рабочие характеристики в диапазоне частот до 100 кГц.

Ключевые слова: катушка индуктивности, экранирование, электромагнитное излучение.

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Introduction

A great threat to the security of information on electronic devices, sensitive elements of various devices, biological objects is created by electromagnetic radiation of various nature. Sources of electromagnetic radiation in everyday life are household appliances, electric vehicles, mobile phones and other electronic devices [1, 2]. To protect against electromagnetic radiation, there are active and passive methods [3]. The passive method is to use screens that absorb or reflect electromagnetic radiation (EMR). For passive protection materials with high magnetic permeability are used. With the help of passive screens it is possible to protect certain sensitive elements of the device, and these screens are easy to use and more profitable in economic terms. However, at the moment there is no unified method for analyzing the effectiveness of shielding. Most scientific papers consider the effect of low-frequency EMR on living organisms and plants without affecting the analysis of the effectiveness of screens.

Analysis of information on the topic of this work shows that there are no standardized generally accepted methods for assessing the effectiveness of shielding [5–7]. To assess the shielding properties of various materials a device or apparatus with a sufficiently powerful emitter of electromagnetic radiation is required which stably operates both with direct and alternating currents of various frequencies. Inductors [8] can be used as such as an emitter, varying the parameters of which the required result can be achieved.

The purpose of this work was to manufacture inductor coils with different parameters, study their characteristics, and determine a sample that provides stable electromagnetic radiation in the frequency range from 25 Hz to 100 kHz. The sample coil with optimal parameters will be used in the hardware-software complex as an emitter and will allow to obtain new, unique data on the shielding efficiency of magnetic coatings and multilayer structures based on them, as well as to compare the previously obtained data on the shielding efficiency in a constant magnetic field with new data that will be obtained with alternating electromagnetic radiation.

Measurement technique

Single-layer and multi-layer inductors were manufactured as prototypes. For the manufacture of single-layer inductors copper wire with a cross section

of 1 and 2 mm was used. The inner diameter (d) of the coils was 7 and 15 mm, the number of turns (N) was from 6 to 41, and the length (l) was from 15 to 65 mm. Multilayer coils were made from copper wire with a diameter of 0.1; 0.18 and 0.35 mm. The coils diameter was 6 mm, the number of turns was from 1000 to 6000, and the length was from 20 to 120 mm. Detailed information about the samples' parameters is presented in Table 1.

Table 1

Parameters of inductors

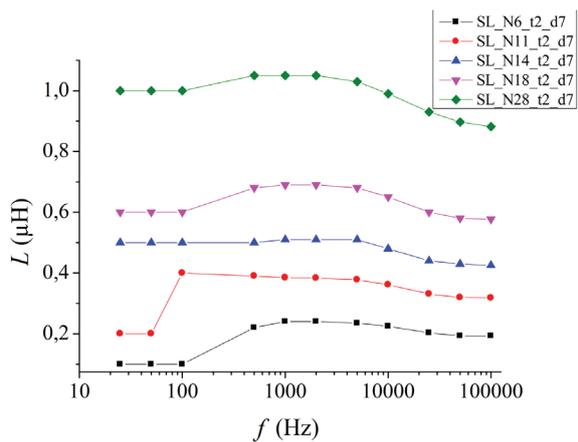
№	Coil designation	d , mm	N	l , mm	t , mm
Single layer coils					
1	<i>SL_N6_t2_d7</i>	7	6	15	2
2	<i>SL_N11_t2_d7</i>	7	11	25	
3	<i>SL_N14_t2_d7</i>	7	14	35	
4	<i>SL_N18_t2_d7</i>	7	18	45	
5	<i>SL_N28_t2_d7</i>	7	28	65	
6	<i>SL_N6_t2_d15</i>	15	6	15	
7	<i>SL_N11_t2_d15</i>	15	11	25	
8	<i>SL_N13_t2_d15</i>	15	13	35	
9	<i>SL_N18_t2_d15</i>	15	18	45	
10	<i>SL_N27_t2_d15</i>	15	27	65	
Multilayer coils					
1	<i>N4-t.1-d6</i>	6	4000	20	0.1
2	<i>N1-t.18-d6</i>	6	1000	19.6	0.18
3	<i>N8-t.15-d6</i>	6	8000	22	0.15
4	<i>N2-t.35-d6</i>	6	2000	70	0.35
5	<i>N4-t.35-d6</i>	6	4000	100	0.35
6	<i>N6-t.35-d6</i>	6	6000	120	0.35

The manufactured samples' parameters, such as inductance (L), active (R) and total resistance (Z) were obtained using an *MNIPi E7-20* emittance meter. In practice, the coils with the optimal parameters calculated theoretically were connected to a current source and amplifier. To detect electromagnetic radiation a multilayer inductor connected to a *UTB-TREND 722-050-5* oscilloscope was used as a signal receiver.

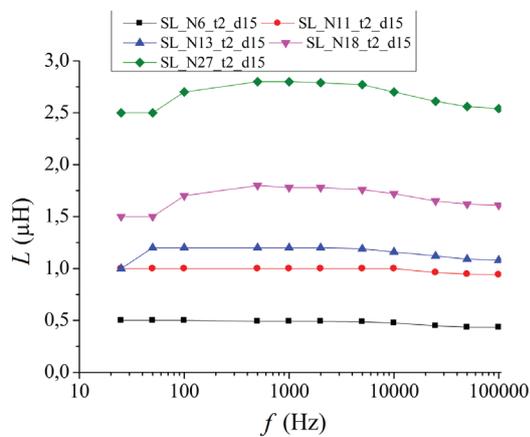
Results and discussion

As can be seen from the graphs (Figure 1), the *SL_N6_t2_d7* coil has the lowest inductance among the coils with an inner diameter of 7 mm. Among

the coils with an inner diameter of 15 mm, the $SL_N6_t2_d15$ coil has the smallest inductance. The inductance of the first sample increases from 0.1 to 0.2 μH in the frequency range from 25 Hz to 100 kHz, while the inductance of the second sample is stable over the entire frequency range and equals 0.5 μH . Despite the large inductance the $SL_N6_t2_d15$ coil looks preferable to the $SL_N6_t2_d7$ one, because it has a constant inductance value over the entire frequency range.



a

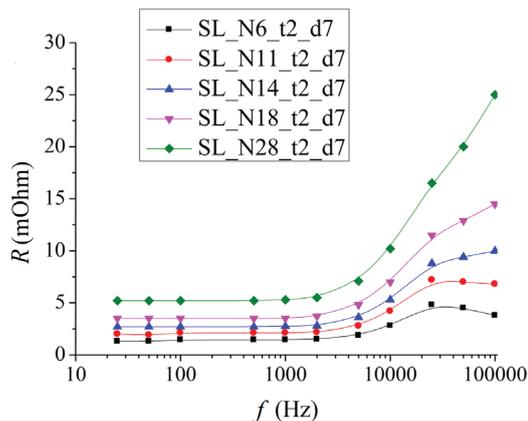


b

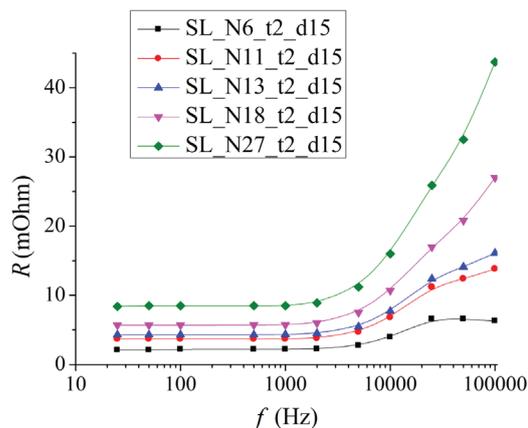
Figure 1 – Dependence of the inductance of single-layer coils on the current frequency: a – coil diameter 7 mm; b – coil diameter 15 mm

Figure 2 shows that all samples with an inner diameter of 7 and 15 mm have constant resistance values R at frequencies from 25 Hz to 5 kHz. After 5 kHz a sharp increase in resistance is observed in almost all samples, with the exception of samples $SL_N6_t2_d7$, $SL_N11_t2_d7$ and $SL_N6_t2_d15$. This is most likely due to the skin effect [9] which

consists in the fact that the currents flowing on the surface of the wire screen the inner layers, as a result of which almost all current is concentrated in a thin surface layer. The proximity effect also contributes, the essence of which is that eddy currents arise in the coil wire under the influence of a magnetic field from adjacent turns [10].



a



b

Figure 2 – Dependence of the resistance of single-layer coils on the current frequency: a – coil diameter 7 mm; b – diameter of coils 15 mm

Figure 3 shows that the total resistance of all coils increases linearly. Coils $SL_N6_t2_d7$ and $SL_N6_t2_d15$ have the lowest total resistance. This is probably due to the fact that these coils have fewer turns, respectively, in their manufacture, a shorter wire length is used compared to the rest of the samples.

These graphs show that the inductance L for coils with a diameter of 7 mm and a wire thickness

of 2 mm does not change significantly at 100 Hz. For coils with a diameter of 15 mm and a wire thickness of 2 mm, as well as for coils with a diameter of 7 mm and a wire thickness of 1 mm, the inductance L practically does not change at frequencies up to 100 kHz.

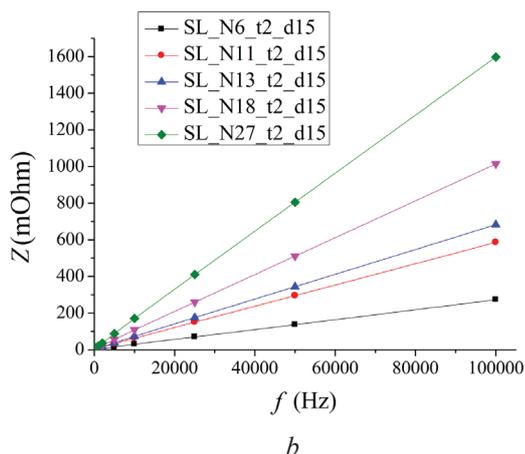
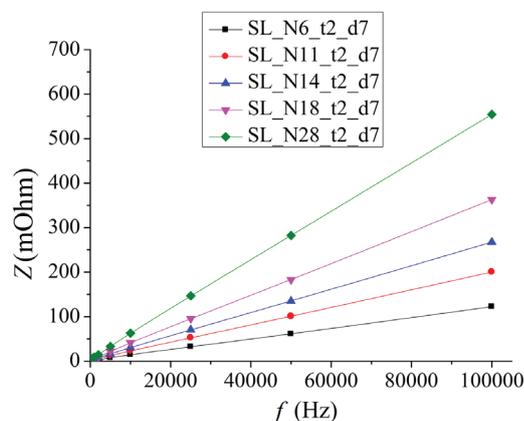


Figure 3 – Graphs of the dependence of the total resistance of single-layer coils on the current frequency: *a* – coil diameter 7 mm; *b* – coil diameter 15 mm

Coils with a diameter of 7 and 15 mm and a wire thickness of 2 mm have less resistance than coils with a diameter of 7 mm and a wire thickness of 1 mm. At the same time, for all coils a slight increase in resistance is observed over the entire frequency range up to 100 kHz. The total resistance of all single-layer coils increases linearly with increasing emitting frequency.

Figure 4 shows that some of the multilayer coils have constant inductance values over the entire frequency sample. The second part of the samples shows unpredictable inductance values. It can be

assumed that this is due to the large number of turns in the coils, some of which may have insulation defects.

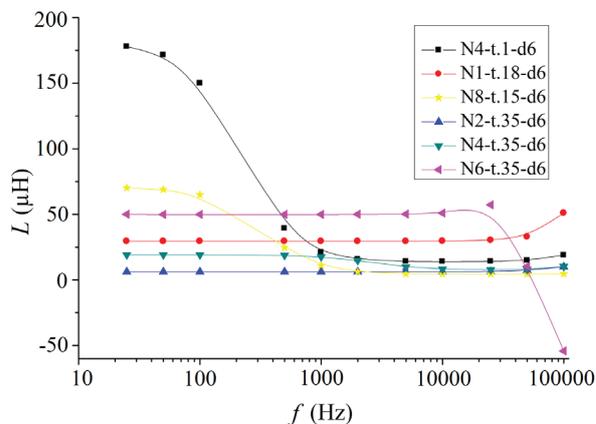


Figure 4 – Graph of the dependence of the inductance of multilayer coils on the current frequency

As seen in Figure 5, the resistance of multilayer coils is constant from 25 Hz to 10 kHz. After 10 kHz, an avalanche-like increase in resistance occurs. Coils *N4-t.1-d6* and *N1-t.18-d6* come into resonance due to the presence of skin and proximity effects. Parasitic capacitances also increase strongly at high frequencies. These capacitances, in combination with the high inductance of the coil, transform it into a whole chain of oscillatory circuits with resonances falling within the operating range or even below it, and then the coil acquires capacitive resistance.

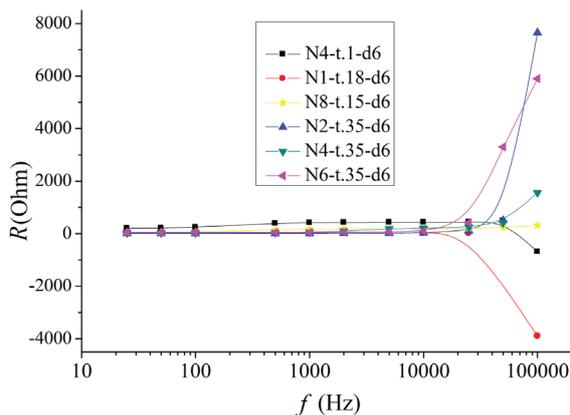


Figure 5 – Dependence of the resistance of multilayer coils on the frequency of the current

Figure 6 presents that the total resistance of all samples has a constant value from 25 Hz to 5 kHz, after 5 kHz there is a rapid increase in the total resistance. This is due to the presence of a skin effect and a proximity effect. These effects are much more

pronounced with multilayer coils, due to the longer winding length and also due to the large number of turns.

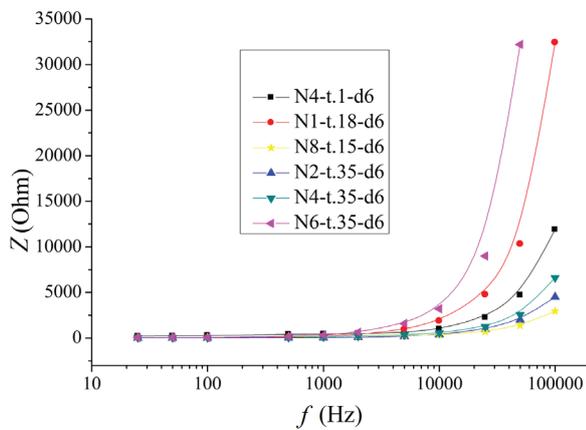


Figure 6 – Dependence of the total resistance of multilayer coils on the frequency of the current

Analyzing the graphs, we can conclude that all multilayer coils for the entire frequency sample

have a constant inductance, except for two samples. At an electromagnetic field frequency of up to 10 kHz, multilayer coils have constant resistance. At a current frequency above 50 kHz, the resistance of all samples begins to increase sharply. The total resistance of the coils begins to increase when the frequency of the electromagnetic field is over 10 kHz.

The values of the magnetic field strength inside the cylindrical coil $H(E)$ for the manufactured samples of inductance coils were calculated by the formula:

$$I = \frac{In}{l},$$

where I – the current in the coil; n – the number of turns of the coil; l – the length of the coil;

$$I = \frac{U}{Z},$$

where U – the voltage applied to the circuit section; Z – impedance measured with an RLC meter.

Table 2

Calculation results of the voltage required to ensure the magnetic field strength of 1, 5, 20 Oe for single-layer coils

№	Coil designation	$U_{1\text{ Oe}}, \text{ V}$		$U_{5\text{ Oe}}, \text{ V}$		$U_{20\text{ Oe}}, \text{ V}$	
		25 Hz	10 kHz	25 Hz	10 kHz	25 Hz	10 kHz
1	SL_N6_t2_d7	0.00026	0.0245	0.0013	0.1225	0.005174	0.48755
2	SL_N11_t2_d7	0.00042	0.04002	0.0021	0.2001	0.0084	0.8004
3	SL_N14_t2_d7	0.00054	0.05346	0.0027	0.2673	0.0108	1.0692
4	SL_N18_t2_d7	0.0007	0.07256	0.0035	0.3628	0.01323	1.371384
5	SL_N28_t2_d7	0.000988	0.105374	0.004836	0.515778	0.01924	2.05202
6	SL_N6_t2_d15	0.00042	0.05468	0.0021	0.2734	0.0084	0.2734
7	SL_N11_t2_d15	0.000648	0.10548	0.003276	0.53326	0.013104	2.13304
8	SL_N13_t2_d15	0.000946	0.150194	0.004644	0.737316	0.01849	2.93561
9	SL_N18_t2_d15	0.00114	0.2028	0.0057	1.0142	0.0228	4.0568
10	SL_N27_t2_d15	0.00042	0.05468	0.002016	0.262464	0.008085	1.05259

For the stable operation of the electromagnetic radiation at different frequencies, it

is required to vary the values of the emitting supplied to the coils. The tables above show the

voltage values calculated to provide magnetic field strengths of 1, 5, 20 Oe in the frequency range

from 25 Hz to 100 kHz, for single-layer and multi-layer coils.

Table 3

Calculation results of the voltage required to ensure the magnetic field strength of 1, 5, 20 Oe multilayer coils

№	Coil designation	$U_{1\text{ Oe}}, \text{ V}$		$U_{5\text{ Oe}}, \text{ V}$		$U_{20\text{ Oe}}, \text{ V}$	
		25 Hz	10 kHz	25 Hz	10 kHz	25 Hz	10 kHz
1	N4-t.1-d6	0.08424	4.76	0.4212	23.8	1.6848	95.2
2	N1-t.18-d6	0.04680	5.13	0.23648	59.2	0.94592	136.8
3	N2-t.35-d6	0.038136	12.6	0.19068	63	0.76272	252
4	N4-t.35-d6	0.05794	13.22	0.2897	66.1	1.1588	264.4
5	N6-t.35-d6	0.08352	42.24	0.4176	211.2	1.6704	844.8

Analyzing the data obtained, we can say that to ensure the operation of multilayer coils, a much higher voltage is required compared to single-layer coils. This is due to the high values of the inductance of multilayer coils as well as the presence of skin and proximity effects. Single-layer coils are also subject to these disadvantages but to a much lesser extent. In addition the voltage values required to operate at 20 Oe of multilayer coils are likely to be critical. Difficulties also arise with the selection of a voltage source operating in such a wide range of values.

Conclusion

Investigations of single-layer and multilayer inductors with different parameters have been carried out.

It was found that it is preferable to use single-layer inductors as a source of electromagnetic radiation operating in the frequency range up to 100 kHz. At a frequency from 10 to 100 kHz, an avalanche-like increase in total resistance begins in multilayer inductors; when measuring the active resistance, some samples enter into resonance. This is due to the presence of skin and proximity effects, which are pronounced in multilayer samples, due to a much larger number of turns, as well as their tightness. The inductance of multilayer coils is 1000 times higher than single-layer coils, as a result of which parasitic capacitances increase significantly. The combination of the factors given above transform a multilayer coil into a chain of oscillatory circuits with resonances often falling into the operating range or below it.

Due to the use of a wire with a cross section of 2 mm for winding single-layer coils, the active resistance of these samples is approximately 1000 times less than that of multilayer coils. Also, due to this fact, much lower values of the applied voltage are required to provide a power of electromagnetic radiation similar to multilayer samples.

Measurements have shown that when the current frequency reaches 5 kHz, a sharp increase in resistance is observed in almost all samples of single-layer coils, with the exception of samples with 6 turns and inner diameters of 7 and 15 mm. It can be assumed that these coils are less susceptible to negative effects due to the fewer turns. A coil with 6 turns and a 7 mm diameter has the lowest inductance value at a current frequency of 100 kHz. However, a sample with 6 turns and a 15 mm diameter has a constant inductance value over the entire frequency range from 25 Hz to 100 kHz. This fact makes the choice in favor of this coil preferable, because the difference in the voltage values required to provide a magnetic field strength of 20 Oe is insignificant.

Reel with optimal parameters planned use as a source of electromagnetic radiation in the hardware and software complex to study the effectiveness of shielding electromagnetic radiation. This hardware and software complex will have a unique structure and characteristics and will allow high-precision studies of the correlation of the chemical composition, structure, and shielding efficiency of a wide range of materials.

In the future, it is planned to conduct research on the influence of various types of cores on the performance of emitting inductors.

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